

High Voltage Gain DC-DC Converter with Reduced Components Voltage Stress for Photovoltaic

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ABSTRACT

In this paper a novel high step up single switch dc dc converter with high efficiency is proposed. In this converter, high voltage gain is achieved using coupled inductor and diode capacitor techniques. Hence, there is no need to use extreme duty cycle. Moreover, the output diode reverse recovery problem has been alleviated in the proposed converter. The voltage stress across all circuit elements has been reduced which decreases the overall size and cost of the proposed converter. Operation principles and steady state analysis of the proposed topology are discussed in detail. Finally, some simulations have been done to verify mathematical derivations and mentioned features of the proposed converter.

Keywords-high voltage gain, reduced switch stress, dc-dc, reverse recovery.

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I. INTRODUCTION

Fuel cell has a slow dynamic response, so the power supply from the fuel cell cannot cope with the power demand during a transient load. Thus, a secondary power source is required to compensate the power difference between the fuel cell and the load, and a battery is generally used to supply a transient power. The power flow between the fuel cell and the battery is managed by a bidirectional dc/dc converter. Conventional isolated/bidirectional dc/dc converters for high-power applications have a voltage-fed full-bridge (FB) (VF-FB) scheme in the high-voltage (HV) side and various current-fed (CF) schemes in the low-voltage (LV) side in general because voltage-fed half-bridge (HB) and voltage-fed push-pull (PP) schemes have disadvantages of high current stress and/or high voltage stress. According to which schemes are used in the LV side, they have several variations such as VF-FB +

two-inductor CF-HB, VF-FB + CF-FB, and VF-FB + CF-PP with six or eight switches. These converters suffer from efficiency decrease at a light-load condition and low efficiency at boost-mode operation due to switching loss. Also, they require a snubber circuit such as an active-clamp circuit to alleviate turn-off voltage spikes in the LV side, which increases the switch number by one or two as a result.

In this letter, a two-stage isolated/bidirectional dc/dc converter adopting a current ripple reduction technique is proposed. The resonant converter with two bridges takes in charge of electrical isolation and constant gain, and the bidirectional control is accomplished using only the second stage with a single bridge. To reduce rms currents in the HV source and link capacitor, capacitor division and synchronizing operation of two stages are adopted.

II. BRIEF REVIEW OF CONTROL TECHNIQUES FOR DC-DC CONVERTERS

DC-DC converters are one of the important electronic circuits, which are widely used in power electronics. The main problem with operation of DC-DC converter is unregulated power supply, which leads to improper function of DC-DC converters. There are various analogue and digital control methods used for dc-dc converters and some have been adopted by industry including voltage- and current-mode control techniques. The DC-DC converter inputs are generally unregulated dc voltage input and the required outputs should be a constant or fixed voltage. Application of a voltage regulator is that it should maintain a constant or fixed output voltage irrespective of variation in load current or input voltage. Various kinds of voltage regulators with a variety of control schemes are used to enhance the efficiency of DC-DC converters.

Today due to the advancement in power electronics and improved technology a more severe requirement for accurate and reliable regulation is desired. This has led to need for more advanced and reliable design of controller for dc-dc converters. There are various types of DC-DC converters required for particular purpose like Buck, Boost, Buck and Boost, Cuk and flyback. These all DC-DC converters have their specific configurations to complete their tasks. Varieties in DC-DC converter required different type of controlling techniques because single technique cannot be applied to all converters as they all have different specifications.

The principal aim of this chapter is to provide an overview of all the control techniques used to facilitate the performance of various kinds of DC-DC converters. In this chapter the basic concept, advantages and disadvantage of each control technique are presented in brief.

Fuzzy logic controller

The nature of Fuzzy control is non-linear and adaptive and it is a practical alternative for a variety of control applications. The concept of Fuzzy Logic (FL) was conceived by Lotfi Zadeh, a professor at the University of California at Berkeley. According to him, it is not as a control methodology, but as a way of processing data by allowing partial set membership function rather than crisp (Fig.2.5). There are four main elements in the fuzzy logic controller system structure named as: Fuzzifier, Rule base, Inference engine and defuzzifier. The working of fuzzy logic controller structure can be

easily understood from the block diagram (Fig.2.5). Its working is divided into 3 main steps: i. Fuzzification. ii. Inference. iii. Defuzzification.

In this process, at the first step a crisp set is used as input data or non-fuzzy data, after this it is converted to a fuzzy set using a fuzzifier by the help of linguistic variables, fuzzy linguistic terms and membership functions.

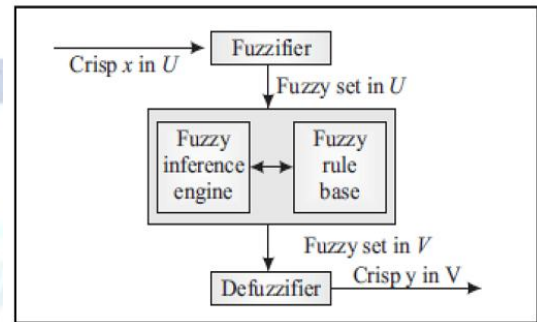


Fig 2.5: Overview of fuzzy logic controller process

The most important thing regarding fuzzy logic is that a numerical value does not have to be fuzzified using only one membership function. Membership functions vary such as Triangular, Gaussian, Trapezoidal, Generalized Bell and Sigmoidal. Rule base is the backbone of fuzzy logic controllers.

Rule Base: i. The purpose of rule base is to control the output variable. ii. A fuzzy rule is a simple IF-THEN rule with a specific condition and conclusion, represented by the matrix table. iii. error and change in error are the two variables taken along the axes, and the conclusions are within the table.

Advantages of Fuzzy Logic Controller: i. Low-cost implementations based on cheap sensors, low-resolution analog-to-digital converter. ii. These systems can be easily upgraded by adding new rules to improve performance or add new features. iii. Fuzzy control can be used for the improvement of traditional controller systems. iv. It provides a robust performance under parameter variation and load disturbances. v. It has a wider range of operating conditions than PID. vi. Can be operated with noise and disturbance of different natures. vii. Developing the fuzzy controller is much cheaper than developing a model-based or other controllers for the same work.

The PWM frequency is important

The PWM is a large amplitude digital signal that swings from one voltage extreme to the other. And, this wide voltage swing takes a lot of filtering to smooth out. When the PWM frequency is close to the frequency of the waveform that you are generating, then any PWM filter will also smooth

out your generated waveform and drastically reduce its amplitude. So, a good rule of thumb is to keep the PWM frequency much higher than the frequency of any waveform you generate.

Finally, filtering pulses is not just about the pulse frequency but about the duty cycle and how much energy is in the pulse. The same filter will do better on a low or high duty cycle pulse compared to a 50% duty cycle pulse. Because the wider pulse has more time to integrate to a stable filter voltage and the smaller pulse has less time to disturb it the inspiration was a request to control the speed of a large positive displacement fuel pump. The pump was sized to allow full power of a boosted engine in excess of 600 Hp.

III. PWM CONTROLLER FEATURES

At idle or highway cruise, this same engine needs far less fuel yet the pump still normally supplies the same amount of fuel. As a result the fuel gets recycled back to the fuel tank, unnecessarily heating the fuel. This PWM controller circuit is intended to run the pump at a low speed setting during low power and allow full pump speed when needed at high engine power levels.

This controller offers a basic "Hi Speed" and "Low Speed" setting and has the option to use a "Progressive" increase between Low and Hi speed. Low Speed is set with a trim pot inside the controller box. Normally when installing the controller, this speed will be set depending on the minimum speed/load needed for the motor. Normally the controller keeps the motor at this Lo Speed except when Progressive is used and when Hi Speed is commanded (see below). Low Speed can vary anywhere from 0% PWM to 100%.

Progressive control is commanded by a 0-5 volt input signal. This starts to increase PWM% from the low speed setting as the 0-5 volt signal climbs. This signal can be generated from a throttle position sensor, a Mass Air Flow sensor, a Manifold Absolute Pressure sensor or any other way the user wants to create a 0-5 volt signal. This function could be set to increase fuel pump power as turbo boost starts to climb (MAP sensor). Or, if controlling a water injection pump, Low Speed could be set at zero PWM% and as the TPS signal climbs it could increase PWM%, effectively increasing water flow to the engine as engine load increases. This controller could even be used as a secondary injector driver (several injectors could be driven in a batch mode, hi impedance only), with Progressive control (0-100%) you could control

their output for fuel or water with the 0-5 volt signal.

Progressive control adds enormous flexibility to the use of this controller. Hi Speed is that same as hard wiring the motor to a steady 12 volt DC source. The controller is providing 100% PWM, steady 12 volt DC power. Hi Speed is selected three different ways on this controller: 1) Hi Speed is automatically selected for about one second when power goes on. This gives the motor full torque at the start. If needed this time can be increased (the value of C1 would need to be increased). 2) High Speed can also be selected by applying 12 volts to the High Speed signal wire. This gives Hi Speed regardless of the Progressive signal.

When the Progressive signal gets to approximately 4.5 volts, the circuit achieves 100% PWM – Hi Speed.

IV. DC – DC CONVERTERS

Modern electronic systems require high quality, small, light weight, reliable, and efficient power supplies. Linear power regulators, whose principle of operation is based on a voltage or current divider, are inefficient. They are limited to output voltages smaller than the input voltage. Also, their power density is low because they require low-frequency (50 or 60Hz) line transformers and filters. Linear regulators can, however, provide a very high quality output voltage.

Their main area of application is at low power levels as low drop-out voltage (LDO) regulators. Electronic devices in linear regulators operate in their active (linear) modes. At higher power levels, switching regulators are used. Switching regulators use power electronic semiconductor switches in on and off states. Since there is a small power loss in those states (low voltage across a switch in the on state, zero current through a switch in the off state), switching regulators can achieve high energy conversion efficiencies. Modern power electronic switches can operate at high frequencies. The higher the operating frequency, the smaller and lighter the transformers, filter inductors, and capacitors. In addition, dynamic characteristics of converters improve with increasing operating frequencies. The bandwidth of a control loop is usually determined by the corner frequency of the output filter. Therefore, high operating frequencies allow for achieving a faster dynamic response to rapid changes in the load current and/or the input voltage. High-frequency electronic power processors are used in dc-dc

power conversion. The functions of dc-dc converters are:

- To convert a dc input voltage V_S into a dc output voltage V_O ;
- To regulate the dc output voltage against load and line variations;
- To reduce the ac voltage ripple on the dc output voltage below the required level;
- To provide isolation between the input source and the load (isolation is not always required);
- To protect the supplied system and the input source from electromagnetic interference (EMI);
- To satisfy various international and national safety standards.

The dc-dc converters can be divided into two main types: hard-switching pulse width modulated (PWM) converters and resonant and soft-switching converters. This chapter deals with the former type of dc-dc converters. The PWM converters have been very popular for the last three decades. They are widely used at all power levels. Topologies and properties of PWM converters are well understood and described in literature. Advantages of PWM converters include low component count, high efficiency, constant frequency operation, relatively simple control and commercial availability of integrated circuit controllers, and ability to achieve high conversion ratios for both step-down and step-up application. A disadvantage of PWM dc-dc converters is that PWM rectangular voltage and current waveforms cause turn-on and turn-off losses in semiconductor devices which limit practical operating frequencies to a megahertz range. Rectangular waveforms also inherently generate EMI.

This chapter starts from a section on dc choppers which are used primarily in dc drives. The output voltage of dc choppers is controlled by adjusting the on time of a switch which in turn adjusts the width of a voltage pulse at the output. This is so called pulse-width modulation (PWM) control. The dc choppers with additional filtering components form PWM dc-dc converters.

Step-Down (Buck) Converter

The step-down dc-dc converter, commonly known as a buck converter, is shown in Fig. 4.4a. It consists of dc input voltage source V_S , controlled

switch S , diode D , filter inductor L , filter capacitor C , and load resistance R . Typical wave form sin the converter are shown in Fig. 4.4b under assumption that the inductor current is always positive. The state of the converter in which the inductor current is never zero for any period of time is called the continuous conduction mode (CCM). It can be seen from the circuit that when the switch S is commanded to the on state, the diode D is reverse biased. When the switch S is off, the diode conducts to support an uninterrupted current in the inductor. The relationship among the input voltage, output voltage, and the switch duty ratio D can be derived, for instance, from the inductor voltage v_L waveform (see Fig. 13.4b). According to Faraday's law, the inductor volt-second product over a period of steady-state operation is zero. For the buck converter

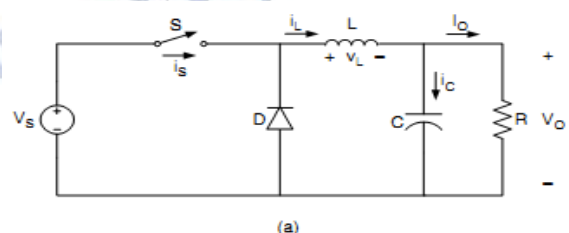
$$(V_S - V_O)DT = -V_O(1 - D)T$$

Hence, the dc voltage transfer function, defined as the ratio of the output voltage to the input voltage, is

$$M_V \equiv \frac{V_O}{V_S} = D$$

It can be seen from above Eq. that the output voltage is always smaller than the input voltage.

The dc-dc converters can operate in two distinct modes with respect to the inductor current i_L . Figure 4.4b depicts the CCM in which the inductor current is always greater than zero. When the average value of the input current is low (high R) and/or the switching frequency f is low, the converter may enter the discontinuous conduction mode (DCM). In the DCM, the inductor current is zero during a portion of the switching period.



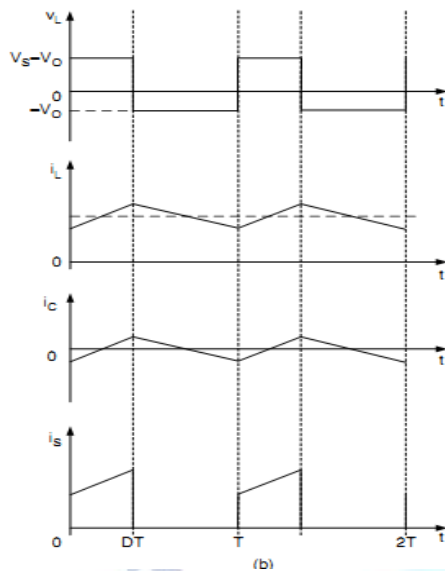


Fig 4.4: Buck converter: (a) circuit diagram and (b) waveforms.

The CCM is preferred for high efficiency and good utilization of semiconductor switches and passive components. The DCM may be used in applications with special control requirements, since the dynamic order of the converter is reduced (the energy stored in the inductor is zero at the beginning and at the end of each switching period). It is uncommon to mix these two operating modes because of different control algorithms. For the buck converter, the value of the filter inductance that determines the boundary between CCM and DCM is given by

$$L_b = \frac{(1-D)R}{2f}$$

Step-Up (Boost) Converter

5a depicts a step-up or a PWM boost converter. It is comprised of dc input voltage source V_S , boost inductor L , controlled switch S , diode D , filter capacitor C , and load resistance R . The converter waveforms in the CCM are presented in Fig. 3.5b. When the switch S is in the on state, the current in the boost inductor increases linearly. The diode D is off at the time. When the switch S is turned off, the energy stored in the inductor is released through the diode to the input RC circuit. Using the Faraday's law for the boost inductor

$$V_S DT = (V_O - V_S)(1-D)T$$

From which the dc voltage transfer function turns out to be

$$M_V \equiv \frac{V_O}{V_S} = \frac{1}{1-D}$$

As the name of the converter suggests, the output voltage is always greater than the input voltage. The boost converter operates in the CCM for $L > L_b$ where

$$L_b = \frac{(1-D)^2 DR}{2f}$$

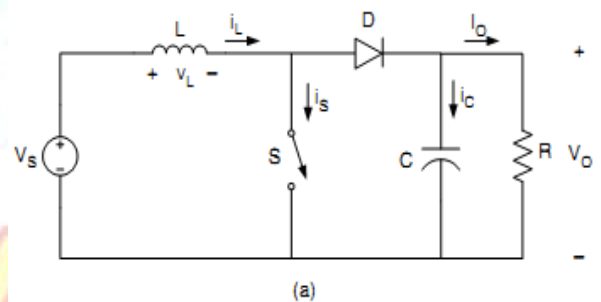


Fig 4.5: Boost converter: (a) circuit diagram and (b) waveforms

V. OPERATION OF HIGH STEP-UP DC-DC CONVERTER

The circuit topology of the proposed converter, which is composed of dc input voltage V_{in} , main switch S , coupled inductors N_p and N_s , one clamp diode $D1$, clamp capacitor $C1$, two capacitors $C2$ and $C3$, two diodes $D2$ and $D3$, output diode D_o , and output capacitor C_o . The equivalent circuit model of the coupled inductor includes magnetizing inductor L_m , leakage inductor L_k and an ideal transformer. The leakage-inductor energy of the coupled inductor is

recycled to capacitor C1, and thus, the voltage across the switch S can be clamped.

The voltage stress on the switch is reduced significantly. Thus, low conducting resistance $R_{DS(ON)}$ of the switch can be used. The original voltage-clamp circuit was first proposed in to recycle the energy stored in the leakage inductor. Based on the topology, the proposed converter combines the concept of switched-capacitor and coupled-inductor techniques. The Switched-capacitor technique in has proposed that capacitors can be parallel charged and series discharged to achieve a high step-up gain. Based on the concept, the proposed converter puts capacitors C2 and C3 on the secondary side of the coupled inductor. Thus, capacitors C2 and C3 are charged in parallel and are discharged in series by the secondary side of the coupled inductor when the switch is turned off and turned on. Because the voltage across the capacitors can be adjusted by the turn ratio, the high step-up gain can be achieved significantly. Also, the voltage stress of the switch can be reduced. Compared to earlier studies, the parallel-charged current is not inrush. Thus, the proposed converter has low conduction loss. Moreover, the secondary-side leakage inductor of the coupled inductor can alleviate the reverse-recovery problem of diodes, and the loss can be reduced. In addition, the proposed converter adds capacitors C2 and C3 to achieve a high step-up gain without an additional winding stage of the coupled inductor. The coil is less than that of other coupled inductor converters.

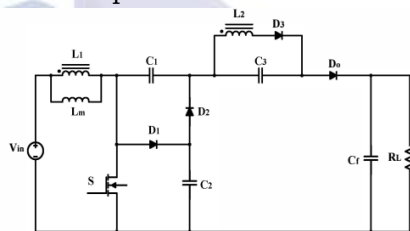


Fig 5.1 high step up dc-dc converter

The main operating principle is that, when the switch is turned on, the coupled-inductor-induced voltage on the secondary side and magnetic inductor L_m is charged by V_{in} . The induced voltage makes V_{in} , V_{C1} , V_{C2} , and V_{C3} release energy to the output in series. The coupled inductor is used as a transformer in the forward converter. When the switch is turned off, the energy of magnetic inductor L_m is released via the secondary side of the coupled inductor to charge capacitors C2 and C3 in parallel. The coupled inductor is used as a transformer in the flyback converter.

To simplify the circuit analysis, the following conditions are assumed.

- 1) Capacitors C1, C2, C3, and C_o are large enough. Thus, V_{C1} , V_{C2} , V_{C3} , and V_o are considered as constants in one switching period.
- 2) The power devices are ideal, but the parasitic capacitor of the power switch is considered.
- 3) The coupling coefficient of the coupled inductor k is equal to $L_m / (L_m + L_k)$, and the turn ratio of the coupled inductor n is equal to N_s / N_p .

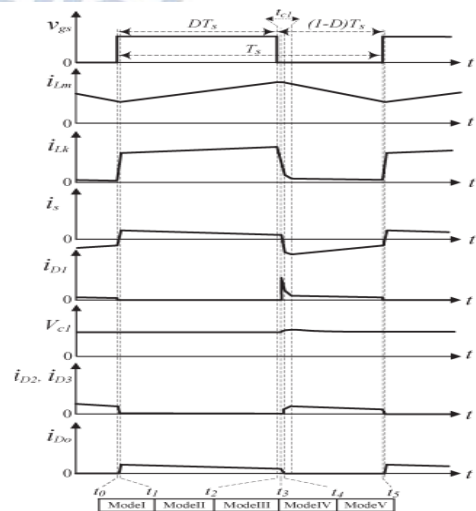


Fig 5.2: waveforms in CCM mode

5.1 CCM Operation

This section presents the operation principle of the proposed converter. The following analysis contains the explanation of the power flow direction of each mode. In CCM operation, there are five operating modes in one switching period. Fig. 5.2 shows the typical waveforms, and Fig. 5.3 shows the current-flow path of each mode of the circuit. The operating modes are described as follows.

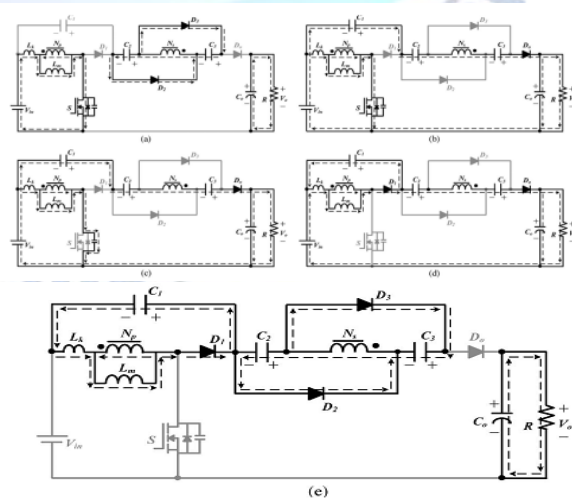


Fig 5.3: Current-flow path of operating modes during one switching period at CCM operation. (a) Mode I. (b) Mode II. (c) Mode III. (d) Mode IV. (e) Mode V

1) Mode I $[t_0, t_1]$: During this time interval, S is turned on. Diodes D1 and Do are turned off, and D2 and D3 are turned on. The current-flow path is shown in Fig. 3.9(a). The voltage equation on the leakage and magnetic inductors of the coupled inductor on the primary side is expressed as $V_{in} = V_{Lk} + V_{Lm}$. The leakage inductor L_k starts to charge by V_{in} . Due to the leakage inductor L_k , the secondary-side current of the coupled inductor is decreased linearly. Output capacitor C_o provides its energy to load R. When current i_{D2} becomes zero at $t = t_1$, this operating mode ends.

2) Mode II $[t_1, t_2]$: During this time interval, S remains turned on. Diodes D1, D2, and D3 are turned off, and Do is turned on. The current-flow path is shown in Fig. 3.9(b). Magnetizing inductor L_m stores energy generated by dc-source V_{in} . Some of the energy of dc-source V_{in} transfers to the secondary side via the coupled inductor. Thus, the induced voltage V_{L2} on the secondary side of the coupled inductor makes V_{in} , V_{C1} , V_{C2} , and V_{C3} , which are connected in series, discharge to high-voltage output capacitor C_o and load R. This operating mode ends when switch S is turned off at $t = t_2$.

3) Mode III $[t_2, t_3]$: During this time interval, S is turned off. Diodes D1, D2, and D3 are turned off, and Do is turned on. The current-flow path is shown in Fig. 3.9(c). The energies of leakage inductor L_k and magnetizing inductor L_m charge the parasitic capacitor C_{ds} of main switch S. Output capacitor C_o provides its energy to load R. When the capacitor voltage V_{C1} is equal to $V_{in} + V_{ds}$ at $t = t_3$, diode D1 conducts, and this operating mode ends.

4) Mode IV $[t_3, t_4]$: During this time interval, S is turned off. Diodes D1 and Do are turned on, and D2 and D3 are turned off. The current-flow path is shown in Fig. 3.9(d). The energies of leakage inductor L_k and magnetizing inductor L_m charge clamp capacitor C_1 . The energy of leakage inductor L_k is recycled. Current i_{Lk} decreases quickly. Secondary-side voltage V_{L2} of the coupled inductor continues charging high-voltage output capacitor C_o and load R in series until the secondary current of the coupled inductor is equal to zero. Meanwhile, diodes D2 and D3 start to turn on. When i_{Do} is equal to zero at $t = t_4$, this operating mode ends.

5) Mode V $[t_4, t_5]$: During this time interval, S is turned off. Diodes D1, D2, and D3 are turned on, and Do is turned off. The current-flow path is shown in Fig. 3.9(e). Output capacitor C_o is

discharged to load R. The energies of leakage inductor L_k and magnetizing inductor L_m charge clamp capacitor C_1 . Magnetizing inductor L_m is released via the secondary side of the coupled inductor and charges capacitors C_2 and C_3 . Thus, capacitors C_2 and C_3 are charged in parallel. As the energy of leakage inductor L_k charges capacitor C_1 , the current i_{Lk} .

VI. MODEL SIMULATION & RESULTS

MATLAB Simulink model for the system under analysis is shown in figure 6.1.

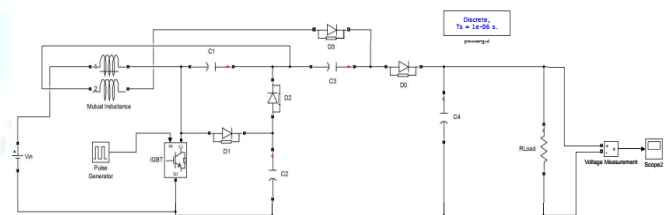


Fig 6.1: MATLAB Simulation model for the circuit under analysis.

Output of DC-DC Boost Converter

The purpose of DC – DC Converter is to provide a stabilized DC Voltage at the input terminals of the inverter. High step up gain can be obtained by using coupled inductor based dc – dc converters. In the proposed circuit a boost converter with a step up gain ratio 6 is used. Output voltage is shown in fig 6.2.

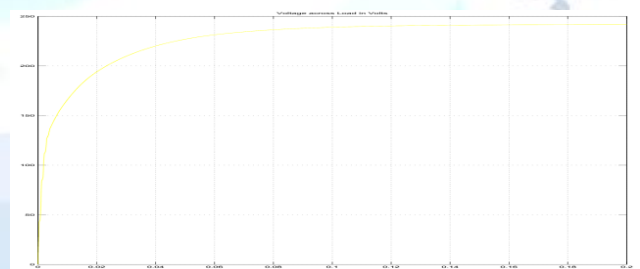


Fig 6.2: Output Voltage of DC – DC Converter.

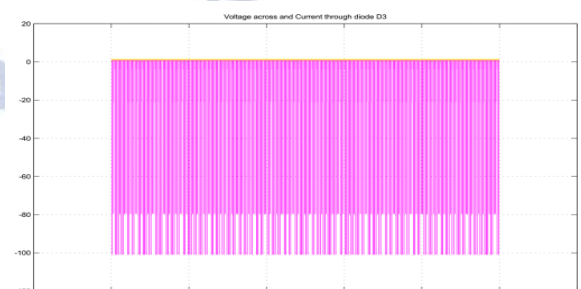


Fig 6.3: Voltage across and current through D3

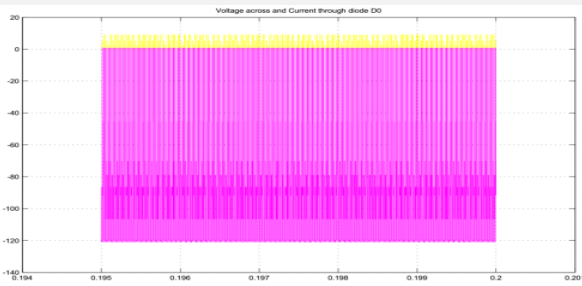


Fig 6.4: Voltage across and current through D0

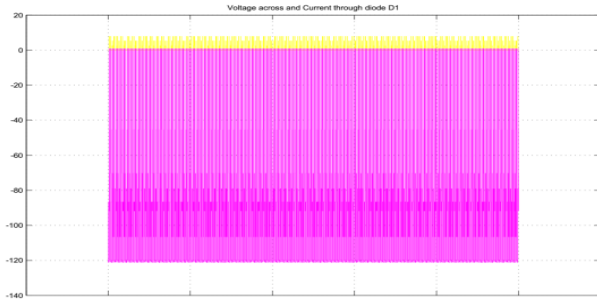


Fig 6.5: Voltage across and current through D1

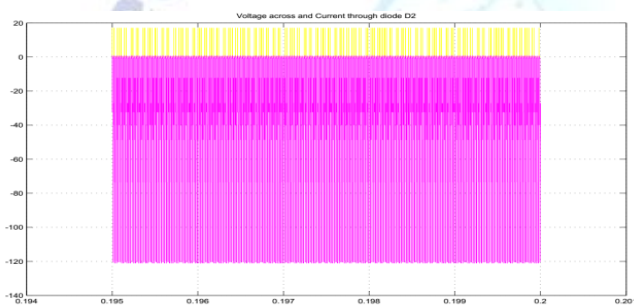


Fig 6.6: Voltage across and current through D2

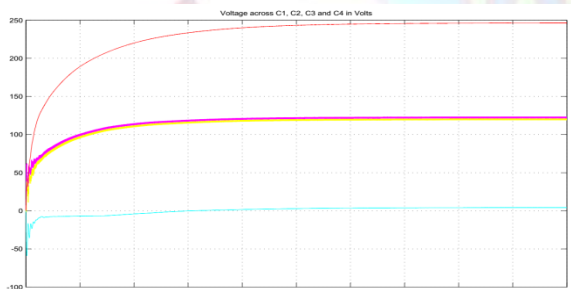


Fig 6.7: Voltage across Capacitors C1, C2, C3 and C4 in Volts

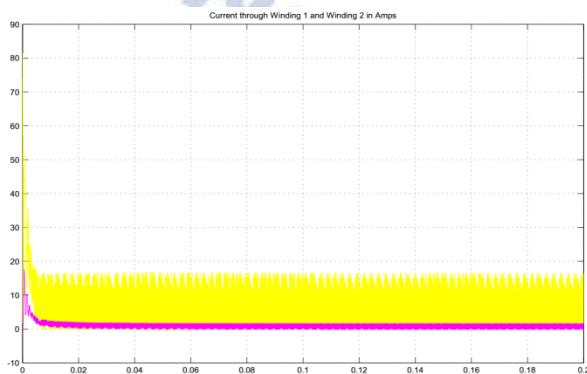


Fig 6.7: Current through coli 1 and coil 2 of coupled inductor in Amps

VII. CONCLUSION

In this paper, a novel high efficiency dc-dc converter with high voltage gain and reduced voltage stress across the switch and other circuit elements has been proposed. Operation principles and steady state analysis have been described.

Furthermore, simulations have been done to verify the performance of the proposed converter. According to Simulation results and the fact that the proposed converter can use components with low voltage ratings, it is obvious that the size and cost of the proposed dc-dc converter can be decreased.

In addition, the reverse recovery problem of the output diode has been alleviated in the proposed converter.

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